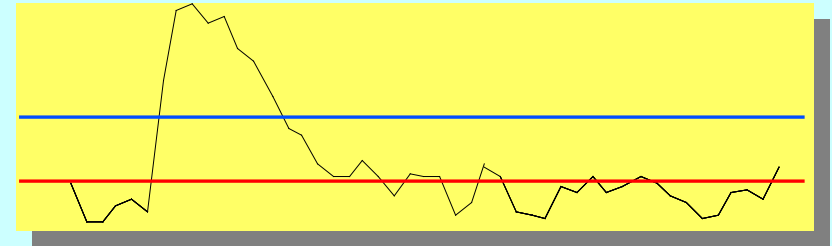


Noise

- **What is NOISE?** A definition:

Any unwanted signal obscuring signal to be observed

two main origins



- **EXTRINSIC NOISE** examples...

pickup from external sources unwanted feedback

RF interference from system or elsewhere, power supply fluctuations

ground currents

small voltage differences => currents can couple into system

may be hard to distinguish from genuine signals *but* **AVOIDABLE**

Assembly & connections, especially to ground, are important

- **INTRINSIC NOISE**

Fundamental property of detector or amplifying electronics

Can't be eliminated but can be MINIMISED

Origins of noise in amplifying systems

•1. Thermal noise

Quantum-statistical phenomenon

Charge carriers in constant thermal motion

macroscopic fluctuations in electrical state of system

•2. Shot noise

Random fluctuations in DC current flow

originates in quantisation of charge

non-continuous current

•3. 1/f noise

Characteristic of many physical systems

least well understood noise source

commonly associated with interface states in MOS electronics

Thermal noise (i)

- Einstein (1906) , Johnson, Nyquist (1928)

e.g. resistor: $\sim 10^{23}$ possible states

macroscopic statistical average over micro-states

- Experimental observation

Mean voltage $\langle v \rangle = 0$

Variance $\langle v^2 \rangle = 4kT.R. f$ $f =$ observing bandwidth

$(v) = \langle v^2 \rangle = 1.3 \cdot 10^{-10} (R. f)^{1/2}$ volts at 300K

e.g. $R = 1M$ $f = 1Hz$ $(v) = 0.13\mu V$

**gaussian distribution
of fluctuations in v**

Noise power = $4kT. f$

independent of R & q independent of f - WHITE

- Quantum effects

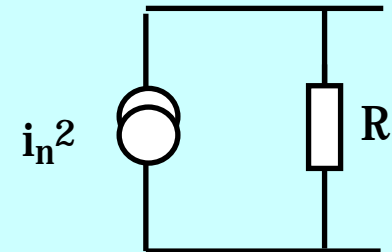
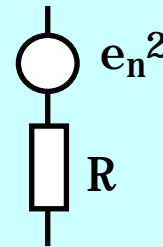
Normal mode energies: kT $hf / (e^{hf/kT} - 1)$ $kT \gg hf$

at 300°K $kT = 0.026$ eV $hf = kT$ at $f = 6.10^{12}$ Hz

Thermal noise (ii)

- **Circuit representations**

Noise generator + noiseless resistance R



- **Spectral densities**

mean square noise voltage or current per unit frequency interval

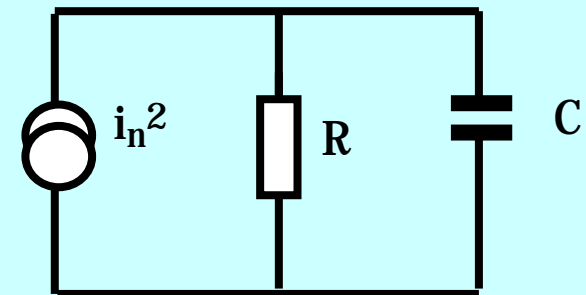
$$w_V(f) = 4kTR \quad (\text{voltage})$$

$$w_I(f) = 4kT/R \quad (\text{current})$$

- **Why not infinite fluctuation in infinite bandwidth?**

A-1: QM formula $\rightarrow 0$ at high f

A-2: real components have
capacitive behaviour (high f)
or inductive (low f).

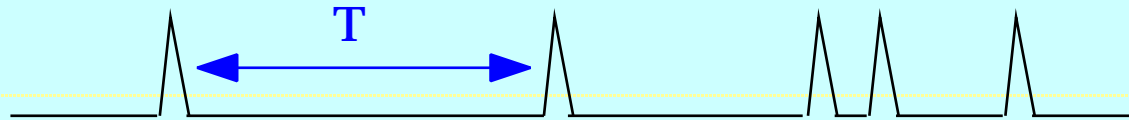


with R and C in parallel $\langle v^2 \rangle = kT/C$

Shot noise

- **Poisson fluctuations of charge carrier number**

eg arrival of charges at electrode in system - induce charges on electrode



quantised in amplitude and time

- **Examples**

electrons/holes crossing potential barrier in diode or transistor

electron flow in vacuum tube

$$\langle i_n^2 \rangle = 2qI \cdot f \quad \text{WHITE} \quad (\text{NB notation } e = q)$$

I = DC current

gaussian distribution
of fluctuations in i

1/f noise

- White noise sources frequently dominate in many real systems

however frequency dependent noise is also common

- 1/f noise is a generic term for a wide range of phenomena, possibly not always related

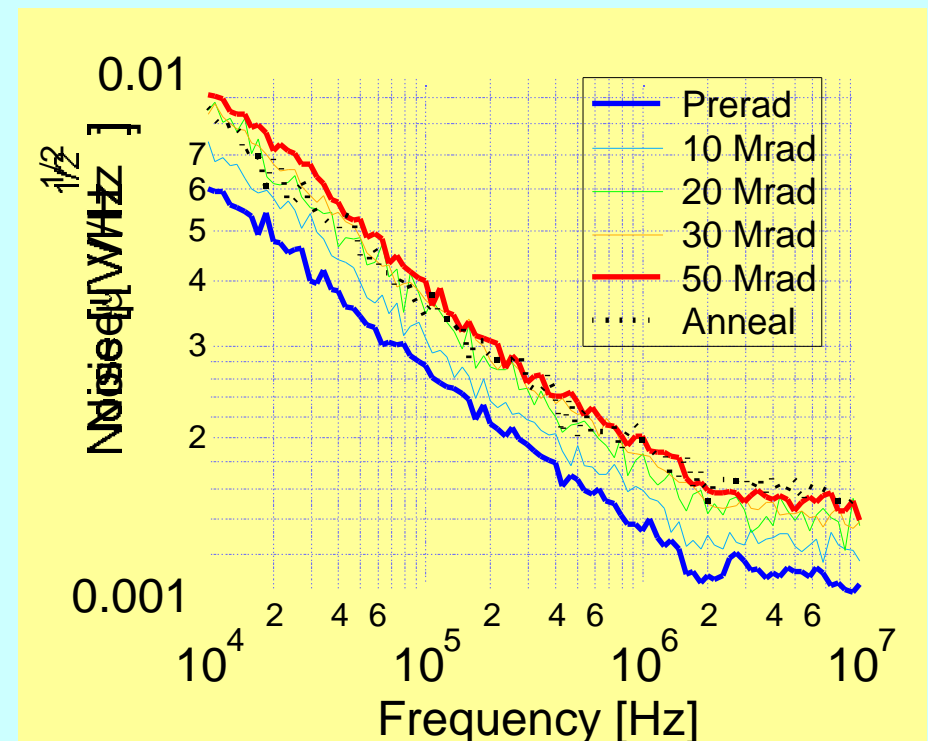
Power spectral density

$$w(f) = A_f / f^n \quad n \sim 0.8-1.5 \text{ typical}$$

- Most important for MOS FET devices, often dominates

but can also arise in other circumstances

e.g. dielectrics,...



pMOS transistor noise spectrum

An explanation for 1/f noise

- Silicon MOS transistors are very sensitive to oxide interface

typically populated by band-gap energy levels (traps)

traps exchange charge with channel - ie. emit and capture electrons or holes

- Traps have lifetime to retain charge $h(t) \sim e^{-t/\tau}$

Expect a range of traps with different time constants, distributed with $p(\tau)$

in frequency domain $H(f) \sim 1/(1+j2\pi f\tau)$

Deduce frequency spectrum by integrating over all values of τ

$$w(f) \sim \int_0^\infty p(\tau) |H(f)|^2 d\tau$$

If $p(\tau) = \text{constant}$, ie all time constants equally probable

$$w(f) \sim \int_0^\infty d\tau / (1 + \tau^2 \omega^2) \quad [\text{standard integral, put } \tan \theta = \tau \omega] \\ = A/f$$

Many other real-life processes have $e^{-t/\tau}$ time distributions -

typical of random, Poisson-type processes

Campbell's theorem - time domain

- Most amplifying systems designed to be linear

$$S(t) = S_1(t) + S_2(t) + S_3(t) + \dots$$

- Impulse response $h(t)$ = response to

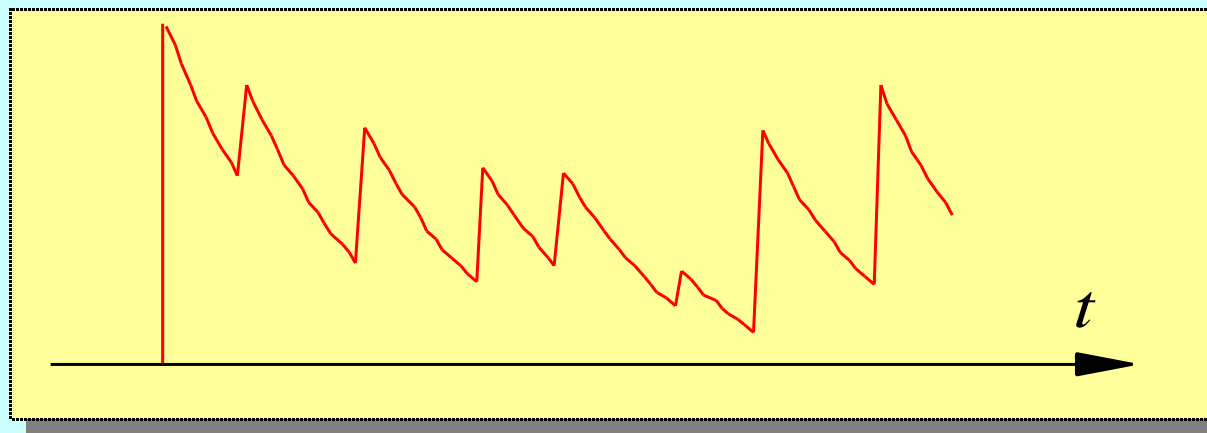


- In a linear system, if random impulses occur at rate n

$$\text{average response } \langle v \rangle = n \int_0^{t_{\text{obs}}} h(t) dt \quad (\text{A})$$

$$\text{variance } \sigma^2 = n \int_0^{t_{\text{obs}}} [h^2(t)] dt \quad (\text{B})$$

i.e. sum all pulses preceding time, t_{obs} , of observation



Campbell's theorem - frequency domain

- Recall relationship between impulse response $h(t)$ and transfer function $H(\omega)$

$$H(\omega) = \int_{-\infty}^{\infty} h(t) \cdot e^{-j\omega t} dt \quad h(t) = \int_{-\infty}^{\infty} H(\omega) e^{j\omega t} d\omega \quad H(\omega) = v_{\text{out}}(\omega) / v_{\text{in}}(\omega)$$

- Rewrite (B) using Parseval's Theorem

$$\int_{-\infty}^{\infty} h^2(t) dt = \int_{-\infty}^{\infty} |H(\omega)|^2 d\omega = 2 \int_0^{\infty} |H(\omega)|^2 d\omega$$

$h(t)$ is real and thus
 $H(-\omega) = H^*(\omega)$

$$\text{so } S^2 = n \int_{-\infty}^{\infty} h^2(t) dt = n \int_{-\infty}^{\infty} |H(\omega)|^2 d\omega$$

This relates noise spectral densities at input and output:

$$w_{\text{out}}(f) = w_{\text{in}}(f) |H(\omega)|^2 \quad \text{can use theorem to calculate system response to noise}$$

- eg. shot noise Consider impulse response to be impulse (ie unchanged!)

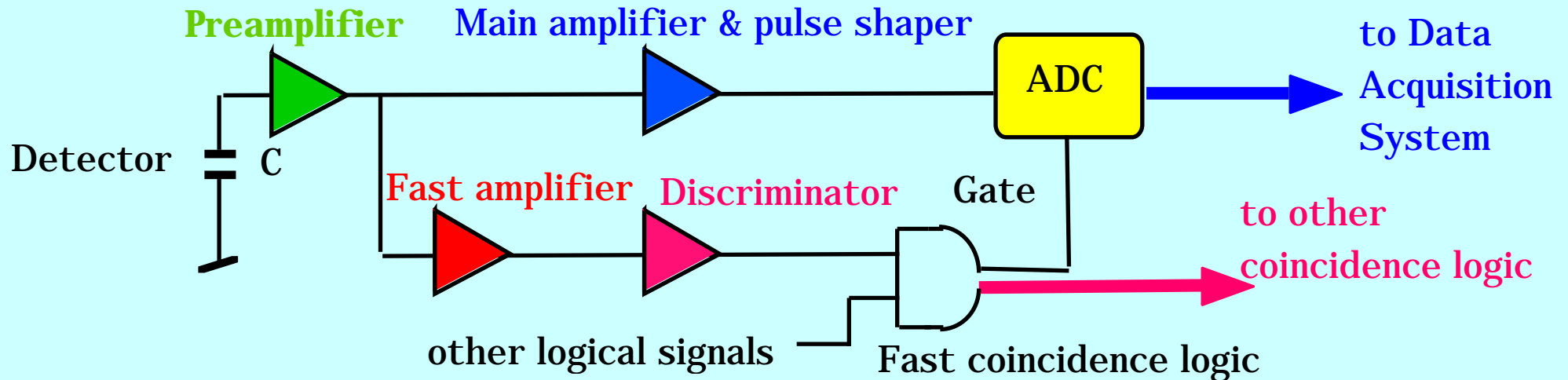
$$h(t) = \delta(t) \Rightarrow H(\omega) = 1$$

$$S^2 = n e^2 \int_{-\infty}^{\infty} \delta^2(t) dt = n e^2 \int_{-\infty}^{\infty} |H(\omega)|^2 d\omega = 2 n e^2 \int_0^{\infty} d\omega$$

$$\text{but } n = I/e \Rightarrow S^2 = \underline{2eI} \int_0^{\infty} d\omega$$

Amplifier systems for spectroscopy

- typical application - precise measurements of x-ray or gamma-ray energies



- pre-amplifier *first stage of amplification*

- main amplifier - *adds gain and provides bandwidth limiting*

ADC - analogue to digital conversion - *signal amplitude to binary number*

- fast amplifier and logic -

start ADC ("gate") and flag interesting "events" to DAQ system

- most signals arrive randomly in time.

Other logic required to maximise chance of "good" event, eg second detector