

Transducers and sensors

- All instruments based on measuring signals

therefore need to understand

the types of signals

properties and characteristics of transducers

applications which are appropriate

impact on the instrument systems

- Transducer

devices which produce an electrical signal proportional to a variable of interest

why? automation for speed, convenience (eg alarm) or objectivity

ease further manipulation of measurements

extend range of processing beyond simple calculations

digital processing now very cheap

- Big area - so which transducers should interest us most? Try to find:

examples of components used for control or monitoring purposes

sensors which exhibit properties of **general interest**,

even if employed for special purposes (like physics research...)

Major transducer types

- Control or measurement

temperature, pressure, humidity, B-field, sound, strain, acceleration,...

growing area of bio-chemical sensors

*beyond scope of these lectures but many common principles
electrical output often desirable for reasons already cited*

- ionisation sensors

general purpose light detection (especially optical communication),

radiation detection (α , β , γ , x-ray, charged particle,...)

many examples of sensors developed for physics which now form components for general use

and vice-versa

specialised state of art instruments often exploit new technologies

Equivalent circuits

- To use any device, we need an effective model of it
should characterise important properties

- Most common & simple picture

Voltage source }
Current source } with associated impedance

this defines how to connect it to a useful circuit

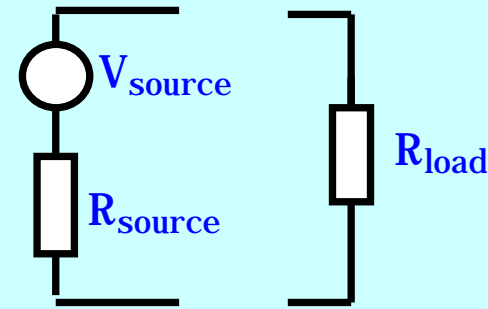
Voltage source

$$i = V_{\text{source}} / (R_{\text{source}} + R_{\text{load}})$$

$$V_{\text{load}} = iR_{\text{load}} = V_{\text{source}} R_{\text{load}} / (R_{\text{source}} + R_{\text{load}})$$

$$\text{if } R_{\text{source}} \gg R_{\text{load}} \quad V_{\text{load}} \ll V_{\text{source}}$$

$$\text{if } R_{\text{source}} \ll R_{\text{load}} \quad V_{\text{load}} \approx V_{\text{source}}$$



we can only sometimes choose R_{source}

*usually defined by transducer - may influence transducer selection
but often transducer chosen first*

we do not always have complete freedom over R_{load}

eg if long cables are required

- **To measure voltages, will often require a high load impedance**

or low source impedance, if intervening circuit

- **Matching**

if $R_{\text{load}} = R_{\text{source}}$ obtain maximum power transfer from source to load

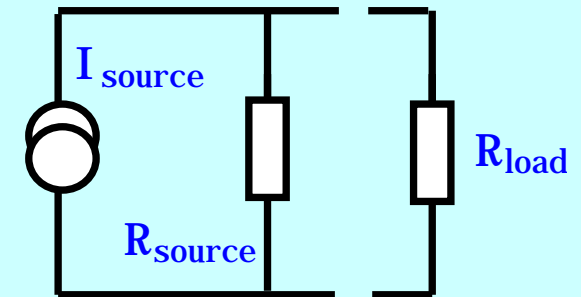
then $V_{\text{load}} = V_{\text{source}}/2$

Current source

$$V_{\text{load}} = I_{\text{source}} (R_{\text{source}} \parallel R_{\text{load}}) = I_{\text{source}} R_{\text{source}} R_{\text{load}} / (R_{\text{source}} + R_{\text{load}})$$

$$I_{\text{load}} = I_{\text{source}} R_{\text{source}} / (R_{\text{source}} + R_{\text{load}})$$

$$\text{if } R_{\text{load}} \ll R_{\text{source}} \quad I_{\text{load}} \approx I_{\text{source}}$$



same comments as previous about ability to choose R_{source} and R_{load}

- **To measure currents, will usually require a low load impedance or high (parallel) source impedance, if intervening circuit**

- **Matching**

$R_{\text{load}} = R_{\text{source}}$ to obtain maximum power transfer from source to load
but this is not always done for practical reasons - discuss later

- **Should note that neither source nor load impedance is always simple resistance**

Temperature measurement

- **Traditional - mercury thermometer**

 - need long, accurately dimensioned tube

 - calibrated scale

 - eg ice, steam*

- **What limits precision? (problem sheet)**

 - accuracy of tube bore

 - practical length of accurate tube

 - operating temperature (melting point of glass?)

 - change in metal dimensions & ability to observe them

 - change in dimensions of tube with temperature

- **Although well developed technology, not very practical for many applications**

 - especially those requiring automation & control

 - cheap, accurate digital thermometers now seem to be widely used in hospitals & for home use - not all electronic*

- **Similar discussion for bi-metallic thermostat**

 - several electronic alternatives are available

Temperature sensor - characteristics required

- Specifications include

Accuracy

probably will depend on T , precision will depend on application, but should be known

Linearity

output (voltage or whatever..) should be $\propto T$ (K, °C, $T-T_0$,..)

Interchangeability

would like to be able to replace the sensor and get similar results

Signal size

ease of measurement

Remote sensing

typically sensor can't be right at source, especially if hot or cold

Temperature range

specs are unlikely to be met from 0K to ∞

Cost

- even if we think of a medical thermometer, these requirements do not change much

Thermocouple

- junction between two different metals can produce a small voltage

value typically very small (10-100 μ V/ $^{\circ}$ C)

depends approximately on difference between two junction temperatures

- one should be reference

well known properties -

so can choose type appropriate to requirement and interchangeable

very convenient for quick, simple measurements

eg control applications

Caveats

*relative measurements excellent but absolute measurements need care
define reference point (& maintain constant!)*

physics of thermocouple

hot wire end produces a temperature gradient

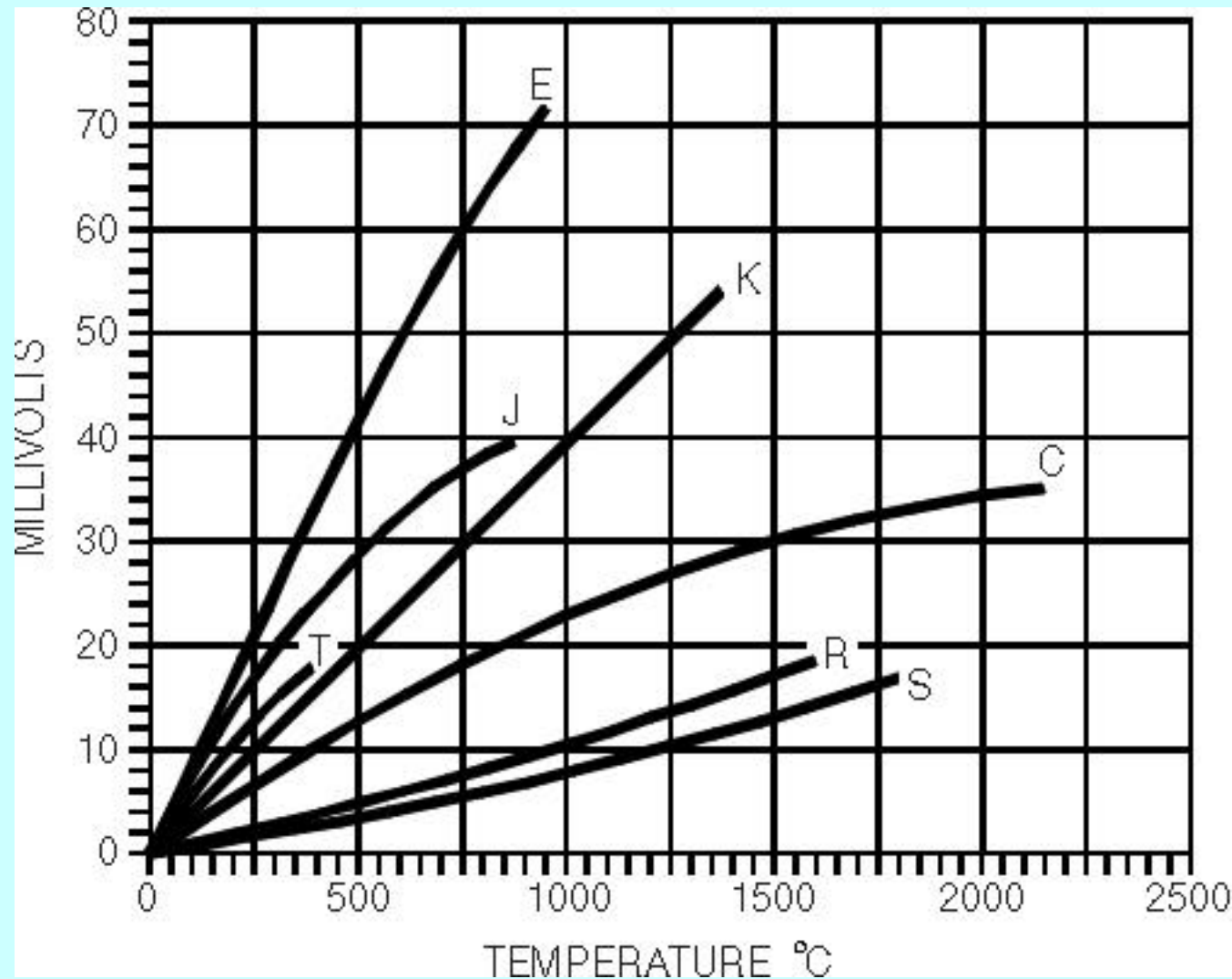
so a carrier density gradient

equilibrium is established when an electric field in the wire balances the carrier diffusion

not practical to put voltmeter across ends of wire - could be hot!

Types of thermocouple (ii)

• www.isi-seal.com/Technical_Info/Tech_Thermocouple.htm



Types of thermocouple

| Type | Metal- 1 | Metal- 2 | Tmax degC | Sensitivity $\mu\text{V}/\text{degC}$ at 20degC | Vout (mV) mV reference junction at 0degC (100 degC) | Vout (mV) mV (400 degC) | Vout (mV) mV (1000 degC) | Rlead /m typical |
|----------|-------------------|---------------------|--------------|---|--|-------------------------------|--------------------------------|------------------------|
| J | Iron | Constantan | 760 | 51.5 | 5.27 | 21.85 | | 12 |
| K | Chromel | Alumel | 1370 | 40.3 | 4.10 | 16.40 | 41.27 | 20 |
| T | Copper | Constantan | 400 | 40.3 | 4.28 | 20.87 | | 10 |
| E | Chromel | Constantan | 1000 | 60.5 | 6.32 | 28.94 | 76.36 | 24 |
| S | Platinum | 90%Pt-10%Rh | 1750 | 5.9 | 0.65 | 3.26 | 9.59 | 6 |
| R | Platinum | 87%Pt-13%Rh | 1750 | 5.8 | 0.65 | 3.41 | 10.50 | 6 |
| B | 94%Pt-6%Rh | 70%Pt-30%Rh | 1800 | 0.0 | 0.03 | 0.79 | 4.83 | 6 |
| C | 95%W-6%Rh | 74%W-26%Rh | 2320 | 25.7 | 2.5 | 10.0 | 25.7 | |
| | Constantan | 55%Cu- 45%Ni | | | | | | |
| | Chromel | 90%Ni- 10%Cr | | | | | | |

- **Junctions are welded by manufacturer**

Often equipped to plug into digital volt meter

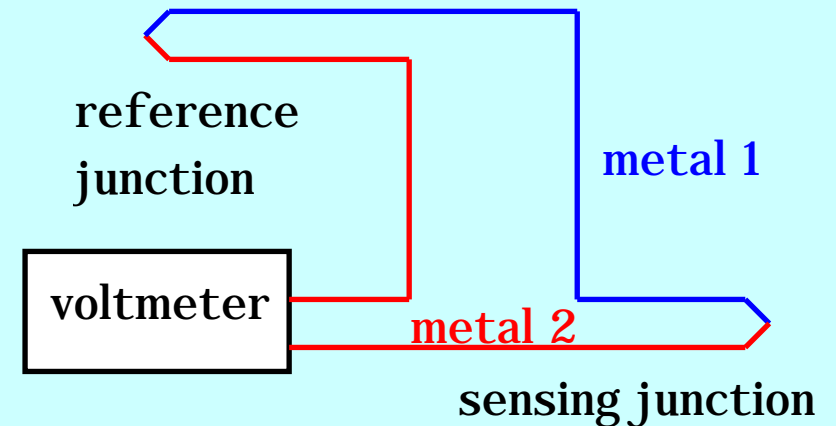
reference to room temperature with internal circuitry

"home-made" systems need care in adding wires -can add another junction

Thermocouple readout

- place reference junction at defined temperature

not practical for most situations



- use compensation circuit to correct for ambient conditions

principle of most temperature meters

= another temperature measuring device needed!

however, not practical to place integrated circuit at hot node!

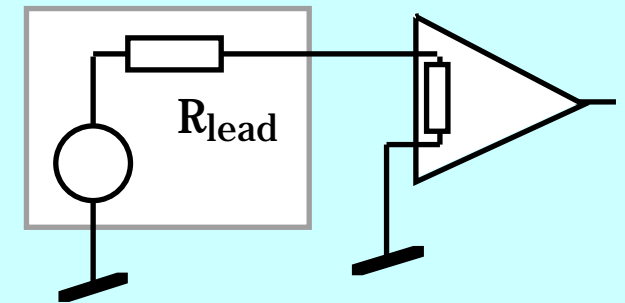
- practical issues

low output voltage to be measured eg $20\text{K} \times 50\mu\text{V}/\text{K} = 1\text{mV}$

measuring amplifier needs careful design to avoid noise

amplifier input resistance should be reasonably high

lead resistance not negligible if long



Thermistor

- **Semiconductor device with well defined R-T characteristic**

coefficient of R vs T $\sim -4\%/^{\circ}\text{C}$ ie. $R/R = \alpha T$

$$R_{\text{typical}} \sim k\Omega$$

precise conformity to standard from manufacturers

range $\sim -50^{\circ}\text{C}$ to $+300^{\circ}\text{C}$

easy to use, with large change in value with temperature

Practical issues

provide current source to operate

accuracy depends on application

non-linear R-T behaviour

accurate applications \Rightarrow careful circuit

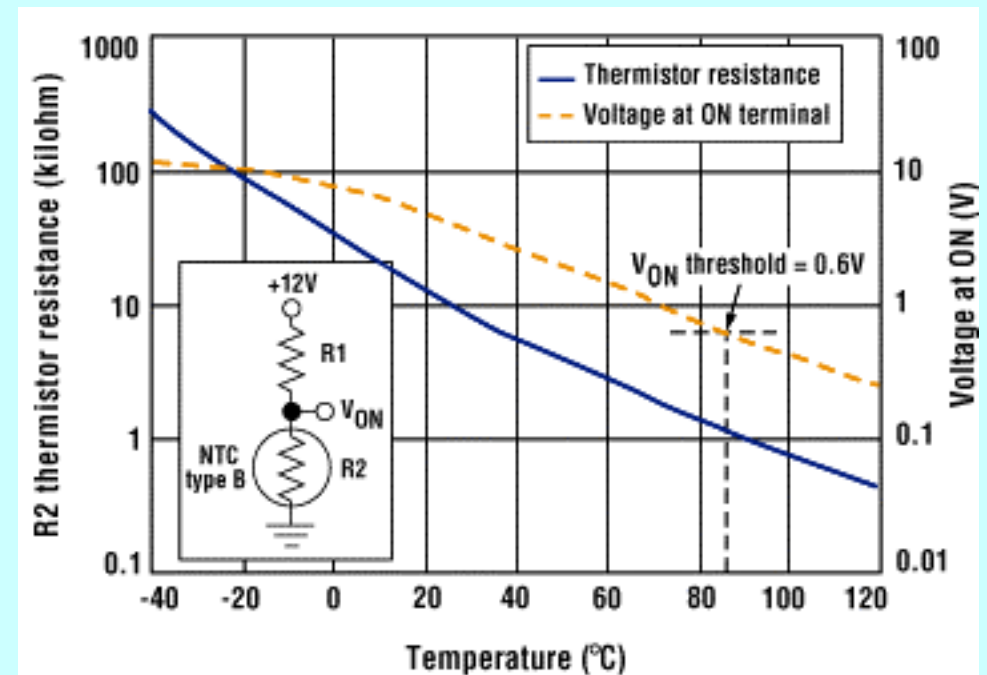
choice (eg balancing bridge)

circuit self-heating can influence

small T - thermal noise could be

concern

need calibration



Temperature ICs

- **Band-gap circuits**

Based on semiconductor junction diode $I \sim \exp(qV/kT)$

- **eg AD590 - discuss more later**

Manufacturer's specs (read them!!)

Two terminal sensor (V_{supply} : +4V to +30V)

Linear output current $1\mu\text{A}/\text{K}$, $\pm 0.3^\circ\text{C}$ over range

T range -55°C to $+150^\circ\text{C}$

Calibrated, with accuracy $\pm 0.5^\circ\text{C}$

Can be used remotely (x100 **feet!**), with long wires

Low cost (£10 for <25)

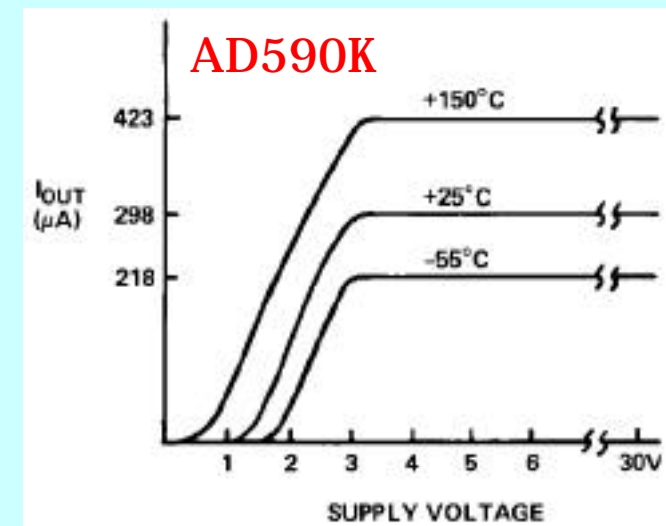
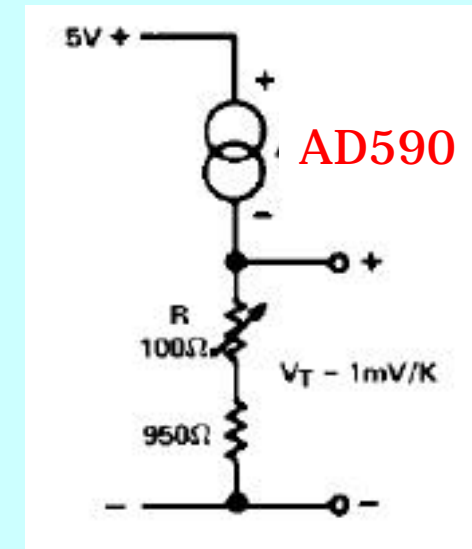
NB several versions

| | Absolute error | Non-linearity |
|---|----------------|---------------|
| J | ± 5.0 | ± 1.5 |
| K | ± 2.5 | ± 0.8 |
| L | ± 1.0 | ± 0.4 |
| M | ± 0.5 | ± 0.3 |

- **Custom ICs -**

can design reference circuits,

eg to save space or remote locations



Platinum resistance

- **Platinum resistance**

Very stable and reproducible, wide T range (~ -200°C to 1000°C)

T coefficient ~ +0.4%/°C

Bulky and expensive for some applications (~ £2-3)

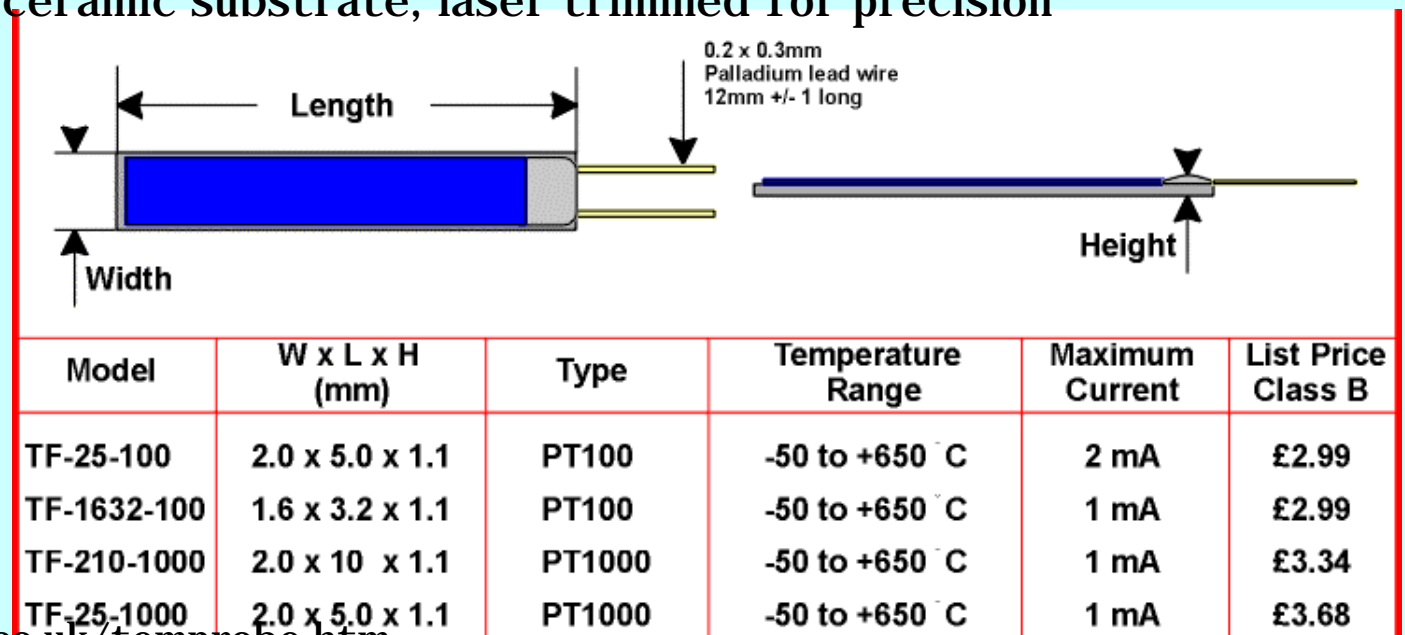
need wires (R) or local I/V circuit

- **Standard value R = 100 (PT100)**

eg Pt film deposited on ceramic substrate, laser trimmed for precision

also

wirewound versions



eg <http://www.kalestead.co.uk/temprobe.htm>

Other temperature transducers

- **Exotics** **each a specialised subject**

Non-contact measurements infra-red sensors based on, eg, CCDs

Ultra-low temperature ~ 0K

Ionisation sensors

- Indirect

produce a signal which must be further converted to an electrical signal
mostly light: scintillators, Cerenkov radiation, transition radiation (x-ray)
acoustic

- Direct

produce a directly measurable electrical signal
may still require amplification
gaseous and semiconductor devices dominate

Scintillators

- **Light emitted following ionisation in a transparent material**

Typical $I(t) \sim I_0 e^{-t/\tau}$ sometimes several components $I_1, I_2, \dots, \tau_1, \tau_2, \dots$

Wavelength of emission determines requirement on photosensor type along with signal speed requirement

eg. $\tau > \mu\text{s} \Rightarrow$ count rates \ll MHz

$\tau \sim \text{ns} \Rightarrow$ count rates \gg MHz

- **Two main material types - contrasting mechanisms**

Inorganic scintillators

result of crystalline structure of material

large band gap \Rightarrow insulators

Organic scintillators

molecular property (independent of state - liquid or solid)

Inorganic scintillators

- ionisation excites electrons from valence to conduction band

de-excitation via photon emission
or radiationless transition

- Large band gap => slow process

low transition probability

short wavelength ($E = E_{\text{bandgap}}$)

- Impurities add centres (traps) in band-gap

increase transition rates

suitable doping can also increase light output

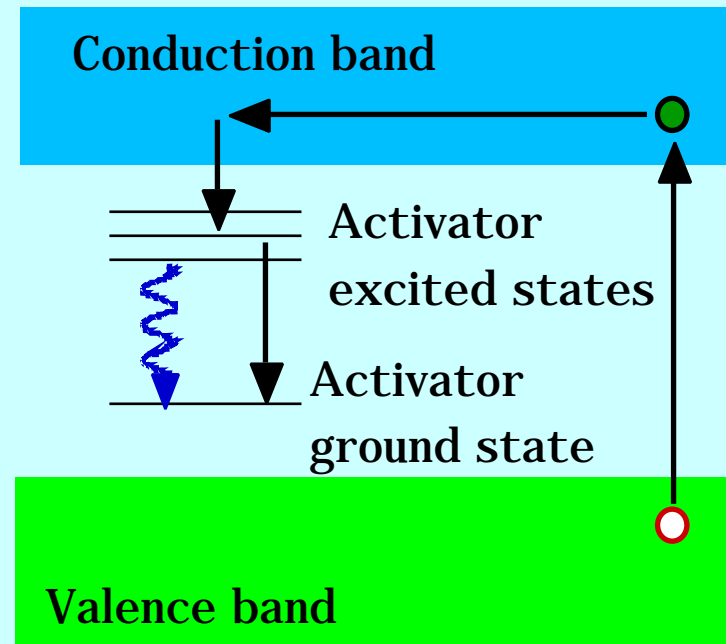
eg thallium in NaI

holes trapped at activator sites

recombination with $e^- \Rightarrow$ photon

smaller energy gap increases wavelength

crystal also transparent to scintillation photons



Inorganic scintillator characteristics

- **high light output but relatively slow ($\sim\mu\text{sec}$), good linearity**

dense, high atomic number (Z) material

good for e^-/gamma ray detection

expensive - very good crystals required, usually large.

raw material, growing, cutting and polishing of large crystals

many require specialised photosensor

blue or UV emission

some undoped materials offer advantages of speed and radiation hardness

drawback of lower light yield

care is needed in material preparation

performance can be badly affected by (wrong!) impurities

some crystals can be coated on photosensors

convenient for efficient sensor systems but limits thickness

- **applications**

medical imaging (eg. gamma camera, $\sim\text{MeV}$ photons from radio-isotopes)

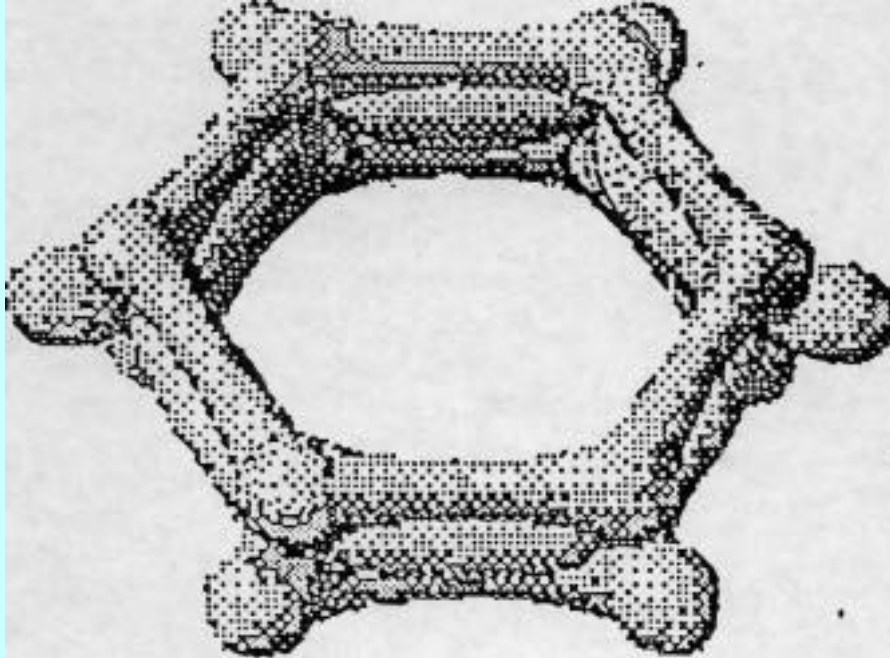
astronomy and particle physics detectors

Examples of inorganic scintillators

| | | peak (nm) | relative light output | time constant (μ sec) | Density g.cm^{-3} | |
|--------------------------|--|--------------|--------------------------|----------------------------------|-------------------------------|---|
| Sodium iodide | NaI (Tl) | 410 | 1 | 0.23 | 3.7 | High light output, hygroscopic, large crystals fragile |
| Caesium iodide | CsI (Tl) | 540 | 1.71 | 0.68 (64%) 3.34 (36%) | 4.5 | Non hygroscopic. wavelength match Si photodiodes |
| Bismuth germanate | BGO $\text{Bi}_4\text{Ge}_3\text{O}_{12}$ | 480 | 0.22 | 0.3 | 7.1 | High Z, low light output |
| Barium fluoride | BaF ₂ (fast) | 220 | 0.05 | 0.0006 | 4.9 | Fast, two components, in UV low light output, rad hard |
| | BaF ₂ (slow) | 310 | 0.16 | 0.62 | | |
| Cerium fluoride | CeF ₃ | 310 340 | 0.005 0.027 | 0.12 | 6.16 | low light output, radiation hard |
| GSO | Gd ₂ SiO ₅ (Ce doped) | 440 | 0.24 | 0.056 (90%) 0.4 (10%) | 6.71 | Fast, rad tolerant |
| YAP | YAlO ₃ (Ce doped) | 440 | 0.47 | 0.027 | 5.37 | Fast, good mechanical properties |

Organic scintillators - hydrocarbon molecules

- Based on excited states of carbon atom, typically electron orbitals of benzene ring (C=C bonds)



imagine orbitals as figures of eight binding two benzene rings but free to move around ring

quasi-free electrons confined to molecular perimeter (length l)

1-d Schrodinger equation $\Rightarrow \psi(x) = \psi(x+l)$

$$E_n = n^2 h^2 / 2me^2 l^2 \quad \text{spectrum of energy levels}$$

In practice more complex, vibrational states give fine structure

range of singlet & triplet states gives both long and short time constants

Organic scintillator spectra

•Complex spectrum of energy levels

major S & P states accompanied by vibrational sub-levels - $E \sim 0.16\text{eV}$

ionisation raises electron to excited state

fast decay to S_{00}

followed by

radiative decay to ground states

= fluorescence $\sim\text{nsec}$

$E_{S_1-S_2} \sim \text{few eV}$

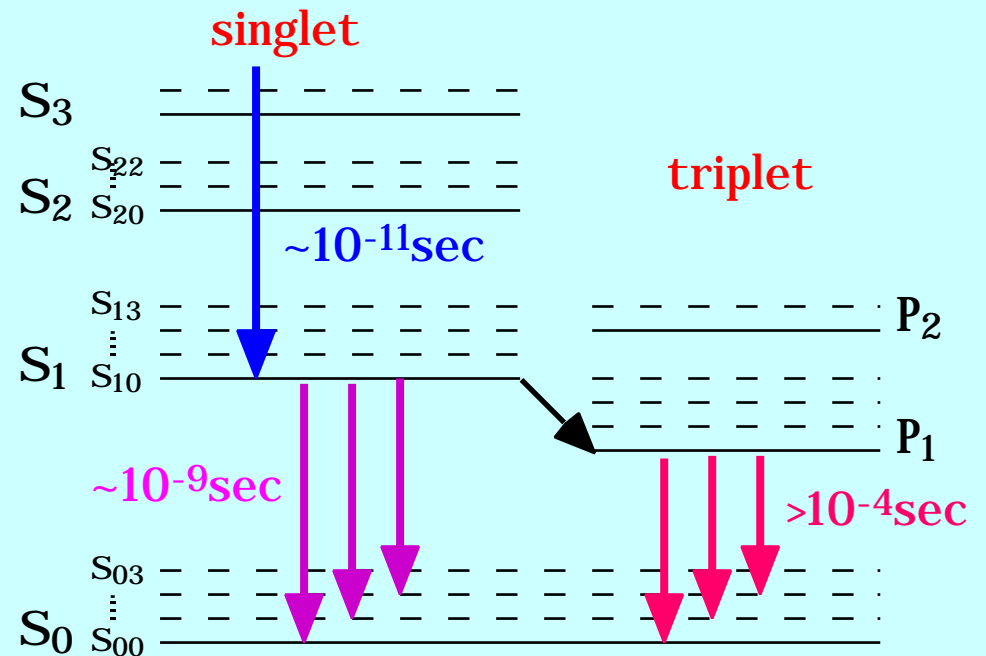
or non-radiative decay S-P

slow and less likely

radiative decay P-S

phosphorescence $\sim\text{msec}$

can also have "delayed fluorescence" from P state thermally excited to S_1

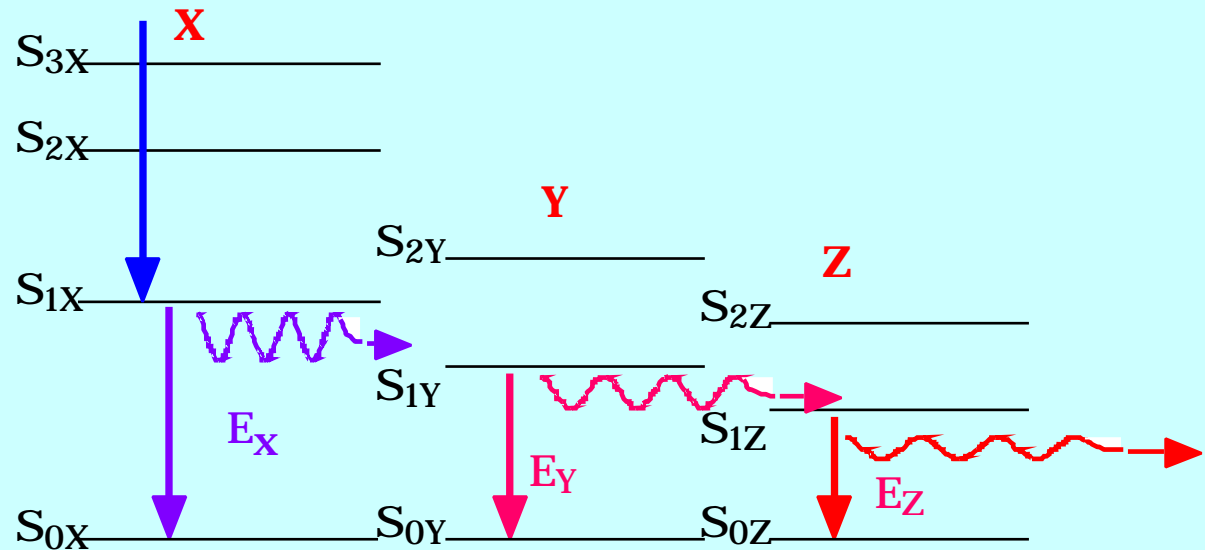


Organic scintillator characteristics

- **Solid base material (plastic) doped with fluor** - but can be liquid scintillator
inexpensive, low Z (primarily C, H, O)
- **Primary fluor likely to be very short wavelength**
not usually matched to available sensors
re-absorption by secondary fluor shifts light to longer, detectable wavelength
overlapping spectra required

Initial photon is absorbed within a few mm, then re-emitted

plastic doped with wavelength shifters converts far-UV light emission to convenient part of spectrum



can be also used to transport light - eg in fibre or plastic light guide

- **multi-step process, including efficiency & attenuation**
low light output cf inorganic scintillators, and non-linear

Examples of organic scintillators

| Primary fluor | peak wavelength nm | time constant ns | relative light output cf NaI |
|---------------|-----------------------|---------------------|---------------------------------|
| Napthalene | 348 | 96 | 0.12 |
| Anthracene | 440 | 30 | 0.5 |
| p-terphenyl | 440 | 5 | 0.25 |
| PBD | 360 | 1.2 | |

Originally discovered in pure natural materials like anthracene but chemists have produced a wide range of binary and tertiary systems

Chemistry of fluors determines and time constants

Wavelength shifter

| | | |
|---------|-----|-----|
| POPOP | 420 | 1.6 |
| bis-MSB | 420 | 1.2 |
| BBQ | 500 | |

Typical commercial products (Nuclear Enterprises)

| | peak wavelength | trise ns | tdecay ns | Attenuation length cm |
|-------|-----------------|-------------|--------------|--------------------------|
| NE110 | 434 | 1.0 | 3.0 | 400 |
| NE104 | 406 | 0.6 | 1.8 | 120 |
| NE108 | 535 | | ~15 | |

Applications

fast detection but without energy measurement, Time of Flight
astro-particle physics, environmental monitoring, nuclear detection

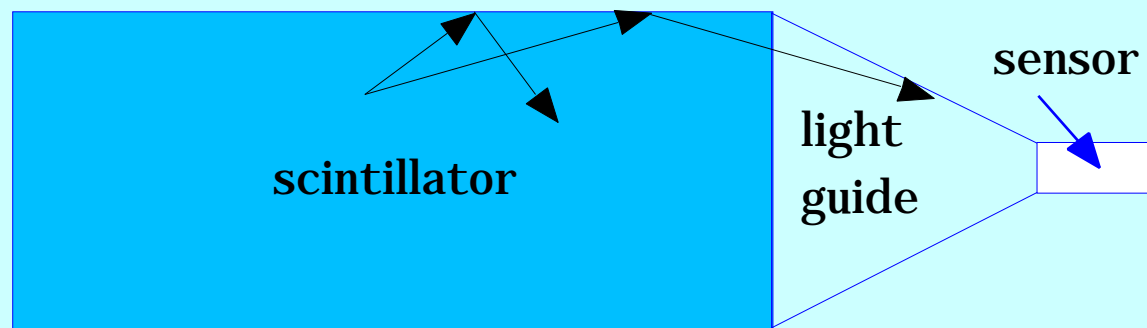
Light collection from scintillators

- **Primary and subsequent emission will be isotropic**

very often require light to be collected on a area much smaller than scintillator

on average, equal light intensity per face

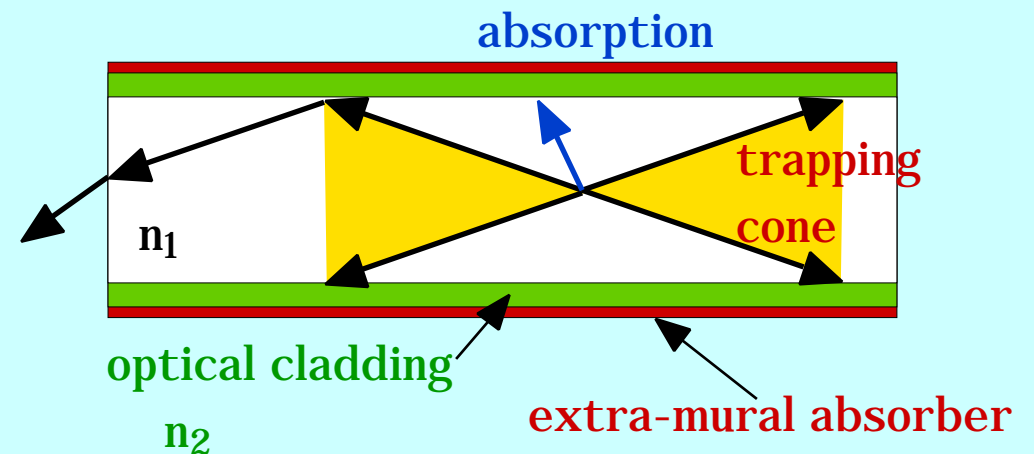
make use of total internal reflection at surface to enhance collection at sensor



eg. loosely wrap scintillator so it has an air-scintillator boundary

for critical applications trace rays to optimise geometry

also used in scintillating optical fibres
same principle for all optical fibre
light transmission



Scintillators - summary

- **Inorganic**

- based on crystals

- important for accurate energy measurement and stopping power

- **Organic**

- molecular property of hydrocarbons

- important for speed and low cost

- **Long term behaviour**

- Both types of scintillator are damaged slowly by radiation

- inorganic - atomic displacement creates new band gap energy levels

- giving attenuation of light

- organic - breaking of chemical bonds alters chemistry

- reduction of light output and attenuation

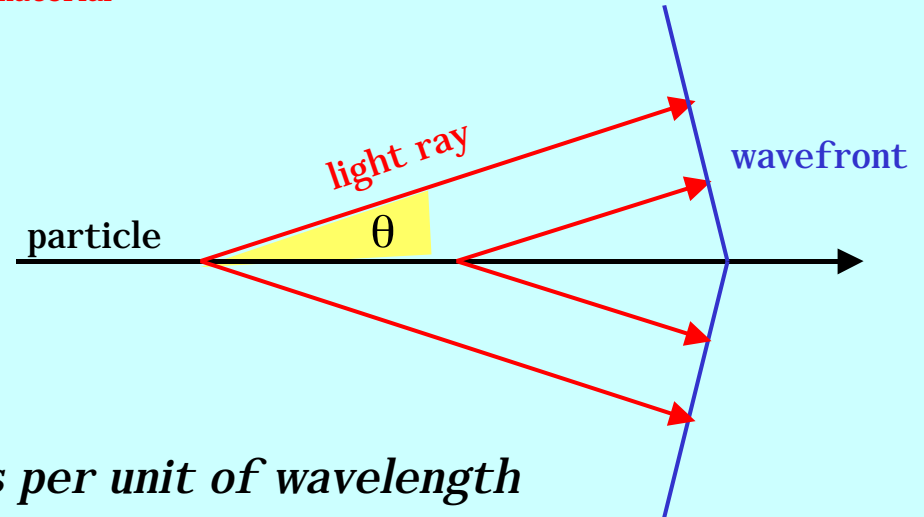
Cerenkov radiation

- when a **charged** particle travels faster than c_{material} in a transparent medium

light emitted on surface of a cone, angle

$$\cos\theta = 1/\beta n$$

$$\beta = v/c \quad n = \text{refractive index}$$



- **Characteristics**

much of light in visible region of spectrum

No of Cerenkov photons per unit thickness per unit of wavelength

$$d^2N/dxd \sim \sin^2 / \lambda^2$$

significant sensitivity gain if extend photon observation to shorter wavelengths

since light output = $f(\lambda)$ possible to distinguish particles of different mass

suitable sensor required

any photon detector with sufficient sensitivity in visible-UV

- **Applications**

identification of particles in accelerator beams and experiments

ultra-high energy particle detection in atmospheric air showers

Examples of Cerenkov radiators

| Radiator | | n | θ_{\max} = 1 | N_0 (cm ⁻¹) 200 < < 750nm |
|-----------------|--------|-------------|------------------------|--|
| He | gas | 1.000035 | 0.48° | 0.11 |
| Air | gas | 1.000283 | 1.36° | 0.94 |
| Isobutane | gas | 1.001270 | 2.89° | 4.3 |
| Aerogel | solid | 1.025-1.075 | 12.7-21.5° | 81-226 |
| Freon | liquid | 1.233 | 35.8° | 575 |
| Water | liquid | 1.33 | 41.2° | 729 |
| Quartz | solid | 1.46 | 46.7° | 892 |
| BGO | solid | 2.15 | 62.3° | 1319 |

Exotics

•Transition radiation

radiation emitted when charged particle crosses dielectric boundary

signals in x-ray region (~ few keV)

very weak radiation - multiple boundaries required to generate measurable signal

but amplitude $\sim \gamma = 1/(1-\beta^2)^{1/2}$ particle ID at very high energy

•Bolometers

large fraction of ionisation energy does not appear as electrical signal

in crystals, eg silicon, excites phonons in crystal = heat

quantum of measurement = energy per phonon \sim meV (10^{-3} eV!)

potential for very high energy resolution

measure change in T $T = E_{\text{deposit}}/C$ C = heat capacity of sensor

$C \sim$ mass so need small sensor and low T (near 0K)

nevertheless, some good results $E_{\text{FWHM}} = 17\text{eV}$ at 0.05K for 6keV x-ray

•Superconducting sensors - several types

two metal superconductors separated by thin insulator layer

under bias, QM tunneling of ionised excited states through insulator

$\epsilon \sim$ meV gives potential for high resolution

Application: particle identification

- A common requirement in nuclear and particle physics is to identify which type of particle is being observed

- stable neutral particles - π^0 , n

very different types of interaction so easy to distinguish- discuss later

- stable or long-lived charged particles: e^- , p^+ , π^\pm , K^\pm , d , He^+ , other ions

typically momentum measurement is made by bending charged particle in B field

$$\text{Force} = q\mathbf{v} \times \mathbf{B} = mv^2/r \quad \Rightarrow \quad r = qB/p \quad \text{if motion in plane perpendicular to } \mathbf{B}$$

direction of bend indicates if charge is + or -

- p and charge are not enough to identify particle, need measurement of m or E

$$E^2 = m^2 + p^2 \quad (c = 1 \text{ units}, m = \text{MeV}/c^2, E = \text{MeV}, p = \text{MeV}/c)$$

Two common methods : Time of Flight & Cerenkov

Time of Flight

- Simply measure time taken between two measurement points, separation L

$$t_1 = L/v_1 \quad t_2 = L/v_2 \quad 1/\beta = E/p = 1 + m^2/2p^2 \quad \text{for } p \gg m$$

$$t = t_1 - t_2 = (L/c)(1/\beta_1 - 1/\beta_2) \quad 3.3\text{ns}(1/\beta_1 - 1/\beta_2) \quad \text{for } L = 1\text{m}$$

Since $\beta \sim 1$, good measurement accuracy required

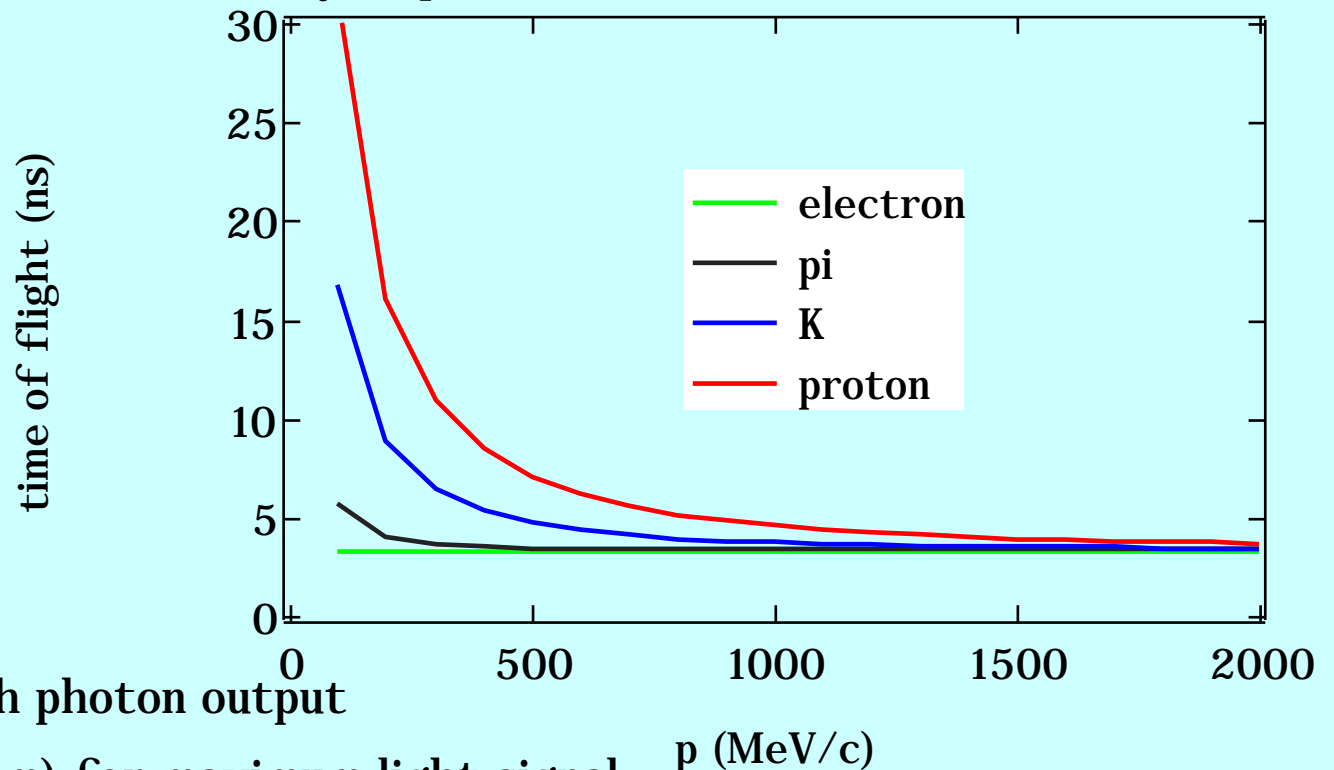
$$t = (L/2p^2c)(m_1^2 - m_2^2)$$

$$m_e = 0.511 \text{ MeV}/c^2$$

$$m_\pi = 140 \text{ MeV}/c^2$$

$$m_K = 494 \text{ MeV}/c^2$$

$$m_p = 938 \text{ MeV}/c^2$$



- Requirements

fast scintillator with high photon output

thick scintillator (~few cm) for maximum light signal

fast response photodetector

Cerenkov identification

• $\cos \theta = 1/n$ so $\beta > 1/n$ for light emission

• light output $N = N_0 L \sin^2 \theta = N_0 L (1 - 1/\beta^2 n^2)$

a good figure of merit $N_0 \approx 100 \text{cm}^{-1}$

depends on details of construction and photosensors

for gaseous radiator $L > 1\text{m}$

still expect small N

• **threshold counters**

binary 0/1 signal

• **ring imaging detectors**

focussing mirror

cone \rightarrow ring

count photons with position sensitive detector

